

A.L.E. method in MOM6

- ALE is an algorithm
 - ALE enables general coordinate models
- MOM6 interpretation of ALE
 - Eulerian (MOM4/5, MITgcm)
 - ALE from CFD
 - ALE in HyCOM and MOM6
- Other details
 - Pressure gradient must be robust in general coordinates
 - High order reconstructions
- Coordinates in MOM6

[Traditional] Eulerian (fixed grid) algorithm

Ignoring inconvenient details such as barotropic mode, diffusion, etc.

$$\begin{aligned}\partial_z p &= -g\rho(z, S^n, \theta^n) && \rightarrow p && \text{Integrate down from top b.c.} \\ v_h^{n+1} &= v_h^n + \Delta t \left(-\frac{1}{\rho_0} \nabla_z p + \dots \right) && \rightarrow v_h^{n+1} \\ \partial_z w &= -\nabla \cdot v_h^{n+1} && \rightarrow w && \text{Integrate up from solid bottom} \\ \theta^{n+1} &= \theta^n - \Delta t \left[\nabla \cdot (v_h^{n+1} \theta^n) + \partial_z (w \theta^n) + \dots \right] && \rightarrow \theta^{n+1} && \text{Explicit vertical transport} \\ &&&&& \text{Conditionally stable}\end{aligned}$$

$$\boxed{\frac{\Delta t w}{\Delta z} < 1}$$

← Implications for topographic representation

Arbitrary Lagrangian Eulerian Method (flavor 1)

Applied only in the vertical direction

Hirt et al. , 1974

$$\partial_z p = -g\rho(z, S^n, \theta^n)$$

$$v_h^{n+1} = v_h^n + \Delta t \left(-\frac{1}{\rho_o} \nabla_z p + \dots \right)$$

(Leclair & Madec, 2011, use this form)

$$\delta_k(w^* + w_g) = -\nabla \cdot h^n v_h^{n+1}$$

Specify motion of grid, w_g , here

$$h^{n+1} = h^n + \Delta t \delta_k(w_g)$$

$$h^{n+1} \theta^{n+1} = h^n \theta^n - \Delta t \left[\nabla \cdot (h^n v_h^{n+1} \theta^n) + \delta_k(w^* \theta^n) + \dots \right]$$

Still have explicit transport

- If $w_g = 0$, then grid is fixed and we recover Eulerian algorithm
- $w^* = w - w_g$ is motion relative to grid
- If we want $w^* = 0$ then we must specify $\partial_z w_g = -\nabla_h \cdot v_h^{n+1}$
- Note that if $w_g \neq 0$ then the grid is moving

Lagrangian phase then remap (flavor 2)

Bleck, 2002

$$\partial_z p = -g\rho(z, S^n, \theta^n)$$

$$v_h^\dagger = v_h^n + \Delta t \left(-\frac{1}{\rho_o} \nabla_z p + \dots \right)$$

$$h^\dagger = h^n - \Delta t \nabla \cdot (h^n v_h^\dagger)$$

← Grid moves
as if $w^* = 0$

$$h^\dagger \theta^\dagger = h^n \theta^n - \Delta t \left[\nabla \cdot (h^n v_h^\dagger \theta^n) \right]$$

← No vertical
transport

- At this point (\dagger), the grid has moved (Lagrangian-ly)
- If the grid is not where we want it, then we remap:

$$h^{n+1} \leftarrow \delta_k Z(z^\dagger) ; \theta^{n+1} = \theta^\dagger(Z(z^\dagger)) ; \dots$$

← It's the
same thing!

- Specifying Z is potentially simpler than specifying w_g

Eulerian and ALE algorithms side-by-side

Eulerian

$$\partial_z p = -g\rho(z, S^n, \theta^n)$$

$$v_h^{n+1} = v_h^n + \Delta t \left(-\frac{1}{\rho_o} \nabla_z p + \dots \right)$$

$$\partial_z w = -\nabla \cdot v_h^{n+1}$$

$$\theta^{n+1} = \theta^n - \Delta t \left[\begin{array}{l} \nabla \cdot (v_h^{n+1} \theta^n) + \\ \partial_z (w \theta^n) + \dots \end{array} \right]$$

$$\boxed{\frac{\Delta t w}{\Delta z} < 1}$$

A.L.E. (flavor 1)

$$\partial_z p = -g\rho(z, S^n, \theta^n)$$

$$v_h^{n+1} = v_h^n + \Delta t \left(-\frac{1}{\rho_o} \nabla_z p + \dots \right)$$

$$\delta_k(w^* + w_g) = -\nabla \cdot h^n v_h^{n+1}$$

$$h^{n+1} = h^n + \Delta t \delta_k(w_g)$$

$$h^{n+1} \theta^{n+1} = h^n \theta^n$$

$$- \Delta t \left[\begin{array}{l} \nabla \cdot (h^n v_h^{n+1} \theta^n) \\ + \delta_k(w^* \theta^n) + \dots \end{array} \right]$$

$$\boxed{\frac{\Delta t w^*}{\Delta z} < 1}$$

$$w^* = w - w_g$$

A.L.E. (flavor 2)

$$\partial_z p = -g\rho(z, S^n, \theta^n)$$

$$v_h^\dagger = v_h^n + \Delta t \left(-\frac{1}{\rho_o} \nabla_z p + \dots \right)$$

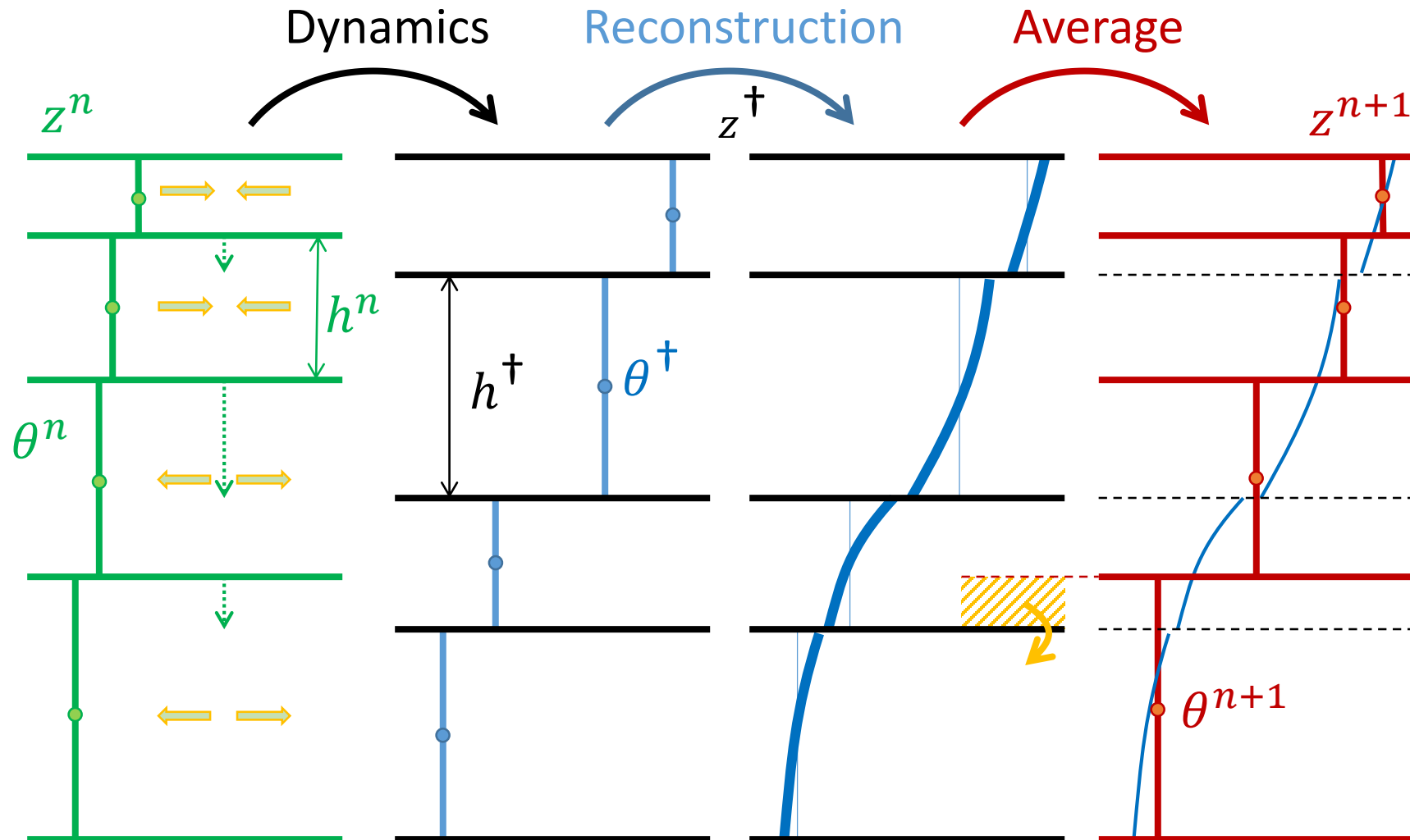
$$h^\dagger = h^n - \Delta t \nabla \cdot (h^n v_h^\dagger)$$

$$h^\dagger \theta^\dagger = h^n \theta^n - \Delta t \left[\begin{array}{l} \nabla \cdot (h^n v_h^\dagger \theta^n) \\ + \dots \end{array} \right]$$

$$h^{n+1} \leftarrow \delta_k Z(z^\dagger)$$

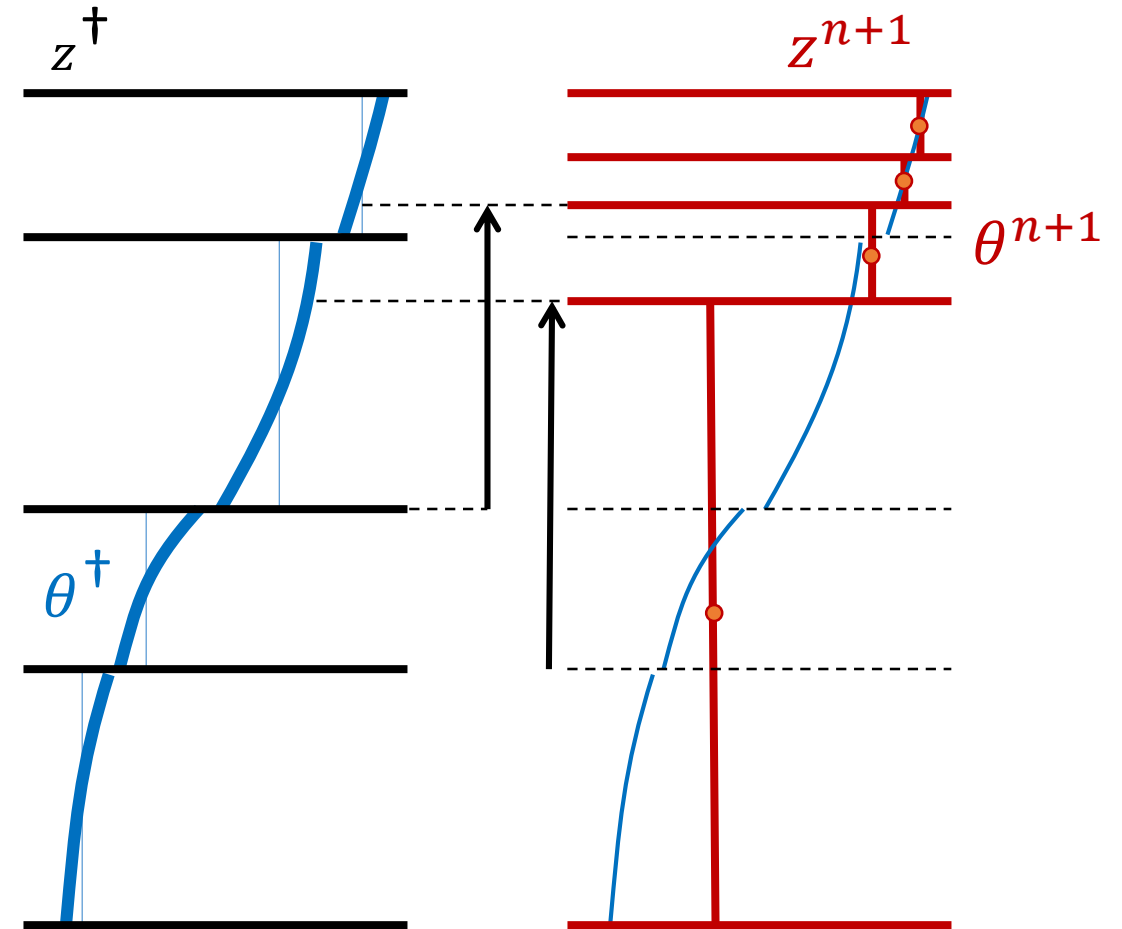
$$\theta^{n+1} = \theta^\dagger(Z(z^\dagger))$$

Full A.L.E. (flavor 2) time step



Stable to “CFL>1” (vertical)

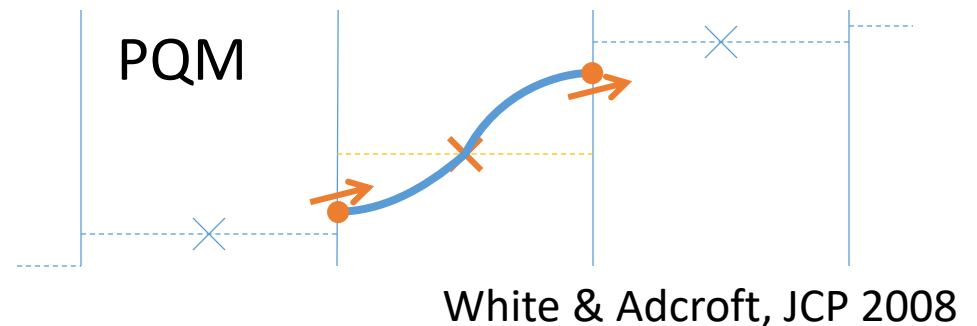
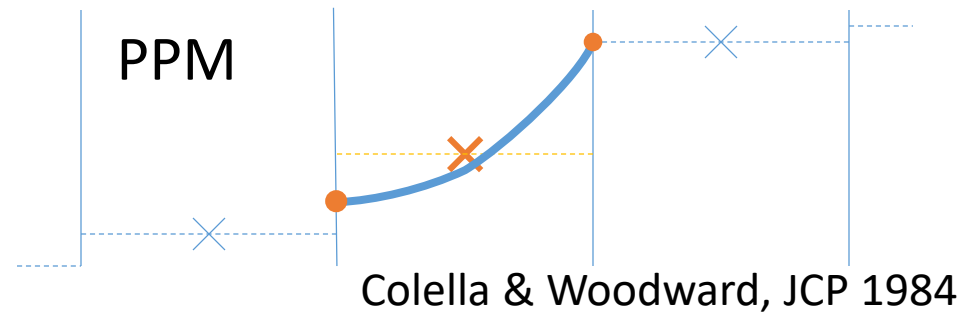
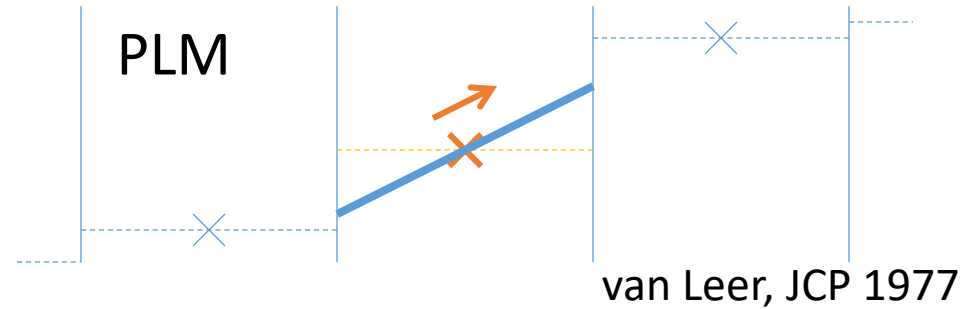
- Target grid, z^{n+1} , can be ANY grid
 - can even have different # of levels
- No restrictions on Δtw_g or Δtw
- Remapping by “projection” works but is prone to non-conservation (roundoff)
- Casting remapping in flux form connects back to flavor 1
 - Remapping equivalent to advection
- Accuracy determined by choice of reconstruction



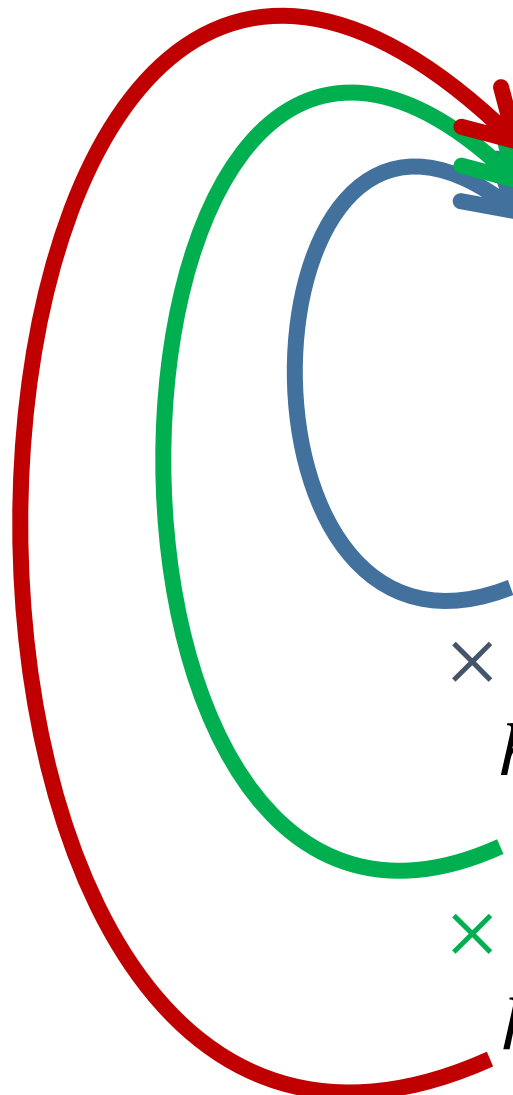
Piecewise * Method (* = C,L,P or Q)

- PLM: two degrees of freedom
 - Cell mean + slope
- PPM: three degrees of freedom
 - Very widely used
 - Cell mean + two edge values
- PQM: five degrees of freedom
 - Cell mean + two edge values + two edge slopes

Successive schemes provide more flexibility to represent structures → more accurate



Sub-cycling dynamics



$$\partial_z p = -g\rho(z, S^n, \theta^n)$$

$$v_h^* = v_h^n + \Delta t \left(-\frac{1}{\rho_o} \nabla_z p + \dots \right)$$

$$h^* = h^n - \Delta t \nabla \cdot (h^n v_h^*)$$

Internal gravity
waves

$$\frac{\Delta t c_g}{\Delta x} < 1$$

$\times M$

$$h^* \theta^* = h^n \theta^n - M \Delta t \left[\nabla \cdot \left(\sum_{m=1}^M h^n v_h^* \theta^n \right) \right]$$

$$\frac{M \Delta t u_h}{\Delta x} < 1$$

$\times N$

$$h^{n+1} \leftarrow \delta_k Z(z^*) ; \theta^{n+1} = \theta^*(Z(z^*)) ; \dots$$

PGF error

- “Analytically” integrate FV PGF
 - Necessary in isopycnal ocean model to avoid thermobaric instability
 - Numerical quadrature more practical

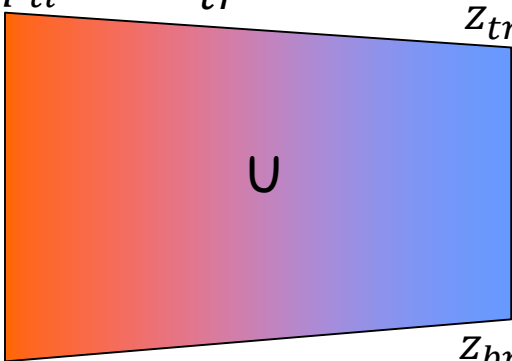


Diagram illustrating a fluid element U with vertical boundaries. The element is a trapezoid with vertices labeled with coordinates and pressures: top-left (z_{tl}, p_{tl}) , top-right (z_{tr}, p_{tr}) , bottom-left (z_{bl}, p_{bl}) , and bottom-right (z_{br}, p_{br}) . The element is colored with a gradient from orange at the bottom to blue at the top.

Integrals of pressure p over vertical boundaries:

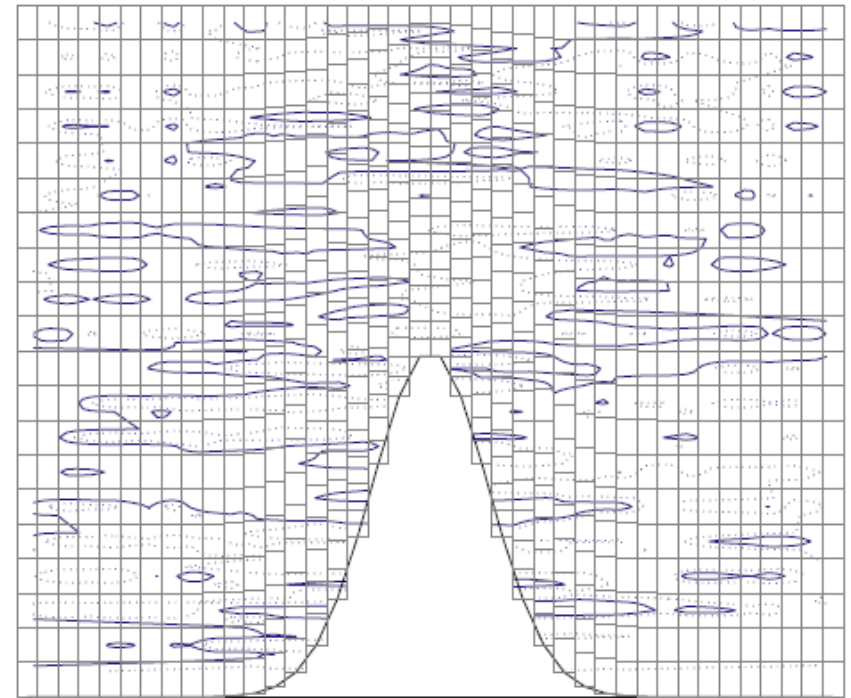
- Left boundary: $\int_{z_{bl}}^{z_{tl}} p \, dz$
- Right boundary: $\int_{z_{br}}^{z_{tr}} p \, dz$
- Top boundary: $\int_{z_{tr}}^{z_{tl}} p \, dz$
- Bottom boundary: $\int_{z_{br}}^{z_{bl}} p \, dz$

Pressure relationships at the boundaries:

$$p_{bl} = p_{tl} + \int_{z_{bl}}^{z_{tl}} g\rho \, dz$$

$$p_{br} = p_{tr} + \int_{z_{br}}^{z_{tr}} g\rho \, dz$$

Seamount resting ocean test



C.I. = 10^{-13} m/s, max $|u| \sim 10^{-11}$ m/s

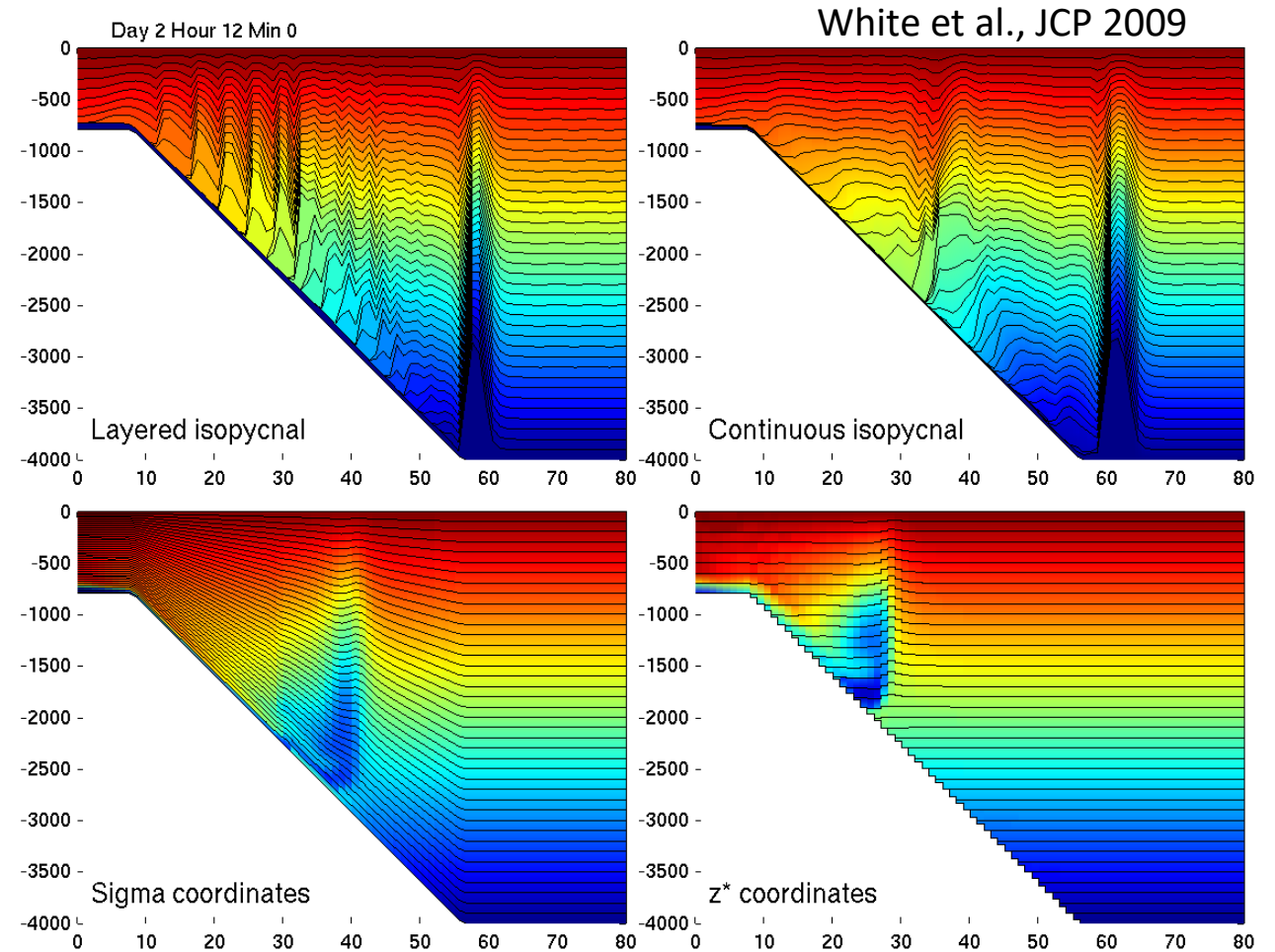
Adcroft et al., 2008; White et al. 2009

Benefits of A.L.E.

- Can explore alternative-/general-/hybrid-coordinates
 - Long running debate about “best” coordinate
(ignore the debate and the question)
 - Adaptive/flexible resolution very useful
- Sub-cycling can offer significant efficiencies
- Accurate and robust to vertical motion
- No need to compromise topography or resolution (unconditionally stable)
- Writing code for general coordinates requires extra thought
 - e.g. parameterizations might be specific to coordinate

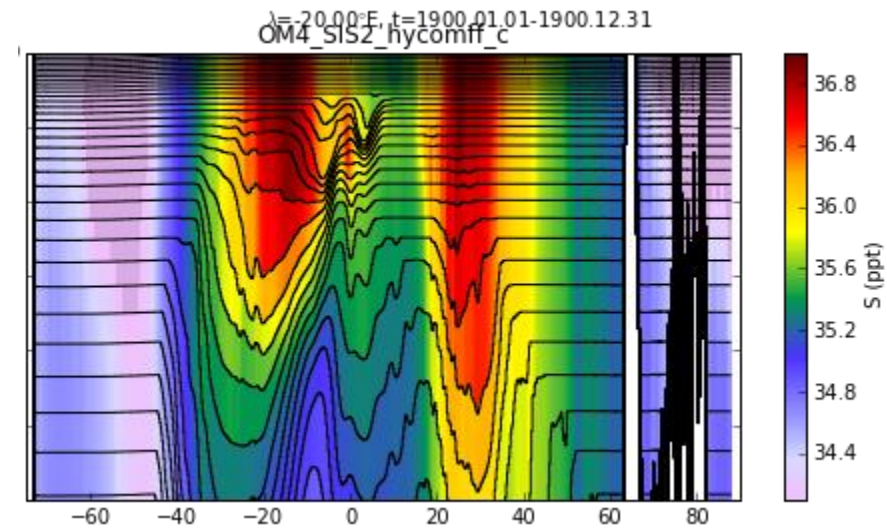
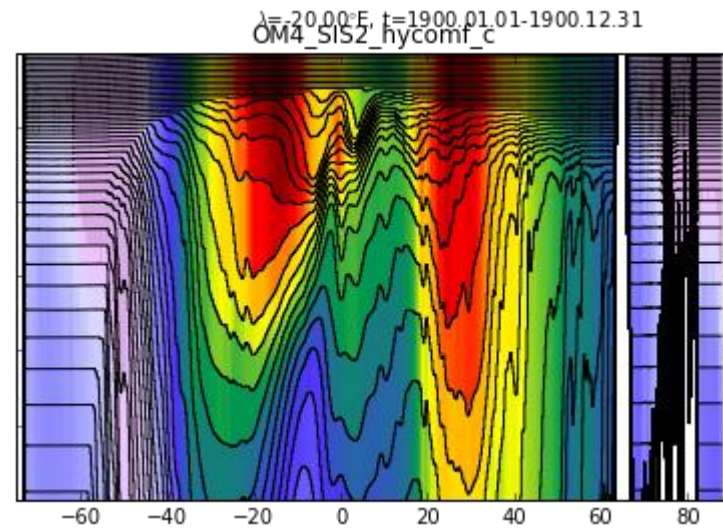
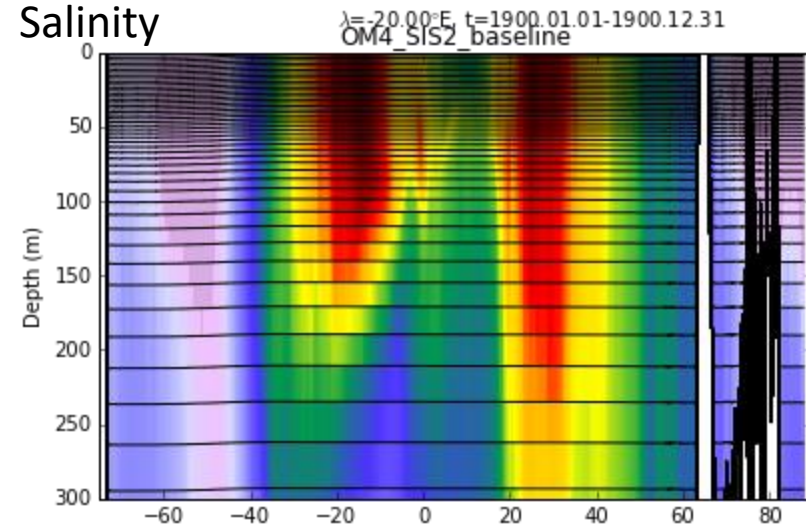
MOM6 coordinates

- Layered isopycnal
 - traditional, not ALE
- Continuous isopycnal (ρ_2)
- Geopotential (z^*)
- Terrain following (σ)
- Hybrid “HYCOM1”
 - Deeper of z^* and ρ_2 for each k
- “SLIGHT”
 - Attempt to use less z^* space than HYCOM1 (not yet successful)
- More to be coded...



Climate drift as function of ocean coordinate

Salinity



Temp
drift

